

3. PUMP

□ NPSHR

NET POSITIVE SUCTION HEAD REQUIRED PUMP MFR
CASING DIMENSION , IMPELLER INLET TYPE , IMPELLER
DESIGN , PUMP FLOW , ROTATIONAL SPEED , LIQUID PERFORMANCE
CURVE NPSHR PLOTTING PUMP 가
 $RPM \propto NPSH^{0.75}$
가 SUCTION HEAD 가 RPM
CRITICAL SUCTION HEAD 가 SYSTEM RPM PUMP

□ NPSHA

NET POSITIVE SUCTION HEAD LIQUID VAPOR PRESSURE
NPSHA CAVITATION PUMP
NPSHA 가 PUMP SUCTION LIQUID FLOW
VAPORIZING VAPOR BUBBLE PUMP CAVITATION
PERFORMANCE
NOISE ERROSION
PUMP SUCTION HEAD PUMP DESIGN
VENDOR NPSHR 2 FEET NPSH
SUCTION PIPING SYSTEM PLUGGING
NONCONDENSIBLE GAS 가 PUMP
SUCTION LIQUID LEVEL , PRESSURE HUNTING SUCTION HEAD
PIPING LAYOUT
SUCTION VESSEL VORTEXING ENTRAINED GAS 가 PUMP

NOZZLE SIZE
NPSHA
$$NPSHA = h_a - h_{vpa} + h_{st} - h_{fs}$$
 h_a = absolute
pressure on suction liquid surface , h_{vpa} = LIQUID VAPOR PRESSURE , h_{st} =
SUCTION LEVEL STATIC HEAD , h_{fs} = SUCTION NOZZLE
FRICTION HEAD LOSS PUMP CENTER LINE

□ DISCHARGE HEAD

PUMP DISCHARGE NOZZLE TOTAL HEAD DISCHARGE FRICTION
HEAD DISCHARGE VESSEL , CONTROL VALVE , DISCHARGE EXIT LOSS

❑ DIFFERENTIAL HEAD

PUMP HEAD SP.GR DATA 가 PRESSURE 가

❑ SPECIFIC SPEED

IMPELLER SPECIFIC SPEED SUCTION SPECIFIC SPEED 가

❑ IMPELLER SPECIFIC SPEED

1 GALLON LIQUID 1 FEET HEAD SPEED
IMPELLER TYPE INDEX HEAD ,
CAPACITY , SUCTION CONDITION , SPEED IMPELLER DESIGN

$$N_s = \frac{\text{rpm} \cdot \sqrt{\text{gpm}}}{H^{\frac{3}{4}}}$$

HEAD 가 SUCTION HEAD 가 SPECIFIC SPEED 가 IMPELLER
HEAD 가 NPSHR SPECIFIC SPEED 가 IMPELLER
SPECIFIC SPEED IMPELLER PUMP SELECTION

BELOW 4,000 - CENTRIFUGAL OR RADIAL TYPE

BETWEEN 4,000 AND 9,000 - MIXED FLOW

ABOVE 9,000 - AXIAL FLOW

SPECIFIC SPEED 가 PROCESS NEED MINIMUM SUCTION HEAD
가

❑ SUCTION SPECIFIC SPEED

SUCTION CAPABILITY IMPELLER DESIGN PARAMETER

$$S = \frac{\text{rpm} \cdot \sqrt{\text{gpm}}}{\text{NPSHR}^{\frac{3}{4}}}$$

S

NPSHR RANGE 3,000 ~ 20,000

IMPELLER DESIGN , SPEED , CAPACITY , LIQUID CAVITATION

HYDROCARBON PUMP 15,000

7,000 ~ 12,000 가

❑ RELATIONS BETWEEN HEAD , HORSEPOWER , CAPACITY , SPEED

BRAKE HORSEPOWER INPUT AT PUMP

$$\text{BHP} = Q \cdot H \cdot (\text{SP. GR}) / 3960 \cdot e$$

IMPELLER DIAMETER

RANGE OPERATING 가

MAX BRAKE HORSEPOWER

$$\text{BHP}(\text{MAX}) = 1.18 \cdot \text{BHP}(\text{AT MAXIMUM EFFICIENCY POINT})$$

DRIVER HORSEPOWER

PUMP

DRIVER INPUT

HORSEPOWER 가 PUMP 가

BHP

COUPLING

LOSS, V-BELT, DRIVER

LOSS

AFFINITY LAWS

1. IMPELLER SIZE EFFICIENCY SPEED, HEAD, BHP

$$Q_2 = Q_1 \left(\frac{n_2}{n_1} \right), H_2 = H_1 \left(\frac{n_2}{n_1} \right)^2, (\text{BHP})_2 = (\text{BHP})_1 \left(\frac{n_2}{n_1} \right)^3$$

SPEED 가

1.5

2. FIXED SPEED, EFFICIENCY DIAMETER, HEAD, BHP

$$Q_2 = Q_1 \left(\frac{d_2}{d_1} \right), H_2 = H_1 \left(\frac{d_2}{d_1} \right)^2, (\text{BHP})_2 = (\text{BHP})_1 \left(\frac{d_2}{d_1} \right)^3$$

IMPELLER SIZE

가 20%

□ TEMPERATURE RISE AND MINIMUM FLOW

PUMP 가

SHUT OFF

FLOW 가

PUMP SUCTION

RETURN

FLOW

가

SUCTION

가

가

SUCTION

CONDITION

PUMP

HARDWARE

DAMAGE

가

MINIMUM FLOW

1. TEMPERATURE RISE IN AVERAGE PUMP DURING OPERATION

$$\Delta T = \frac{(1 - e) \cdot H}{778 \cdot C_p \cdot e}$$

2. TEMPERATURE RISE AT SHUT OFF

$$\text{Temp. rise (F / min)} = \frac{\text{BHP at shut off} \cdot 42.4}{\text{weight of liquid in pump} \cdot C_p}$$

3. MINIMUM FLOW

5 STEP

STEP 1 : NPSH

STEP 2 : NPSH + VAPOR PRESSURE AT SUCTION CONDITION

VAPOR

PRESSURE 가

(T2)

STEP 3 : ALLOWABLE TEMPERATURE RISE = T2 - ACTURAL PUMPING TEMPERATURE.

STEP 4 : MINIMUM SAFE CONTINUOUS FLOW EFFICIENCY

$$e = \frac{\text{H at shut off from curve}}{778 \cdot Dt \cdot C_p + \text{H at shut off}}$$

STEP 5 : PERFORMANCE CURVE

STEP4

EFFICIENCY

FLOW

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